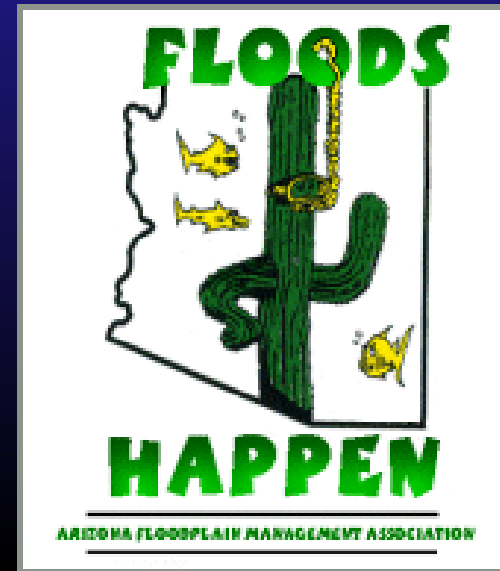
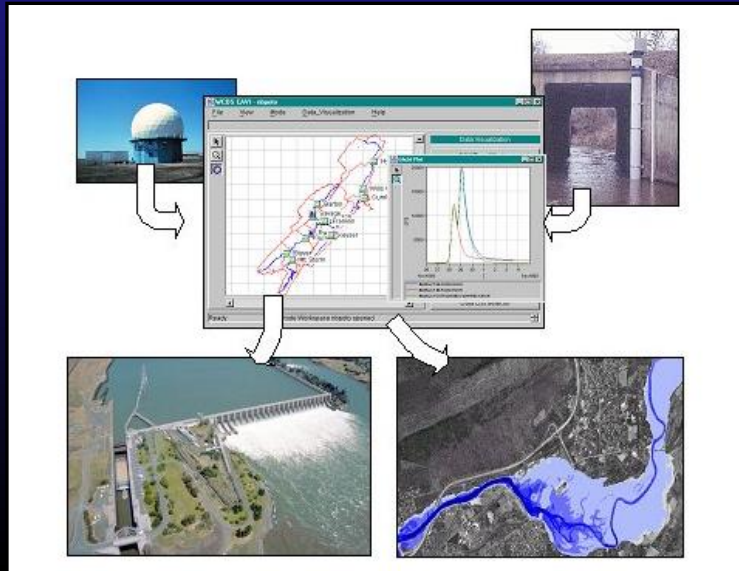


U.S. Army Corps of Engineers' CorpsWaterManagementSystem : CWMS



Chuck Davis, CFM – WEST Consultants, Inc.
Darren Bertrand – WEST Consultants, Inc.

Presentation Overview

- Brief overview of CWMS
- Synopsis of the Modules and Components
- Overview of the Santa Ana River CWMS

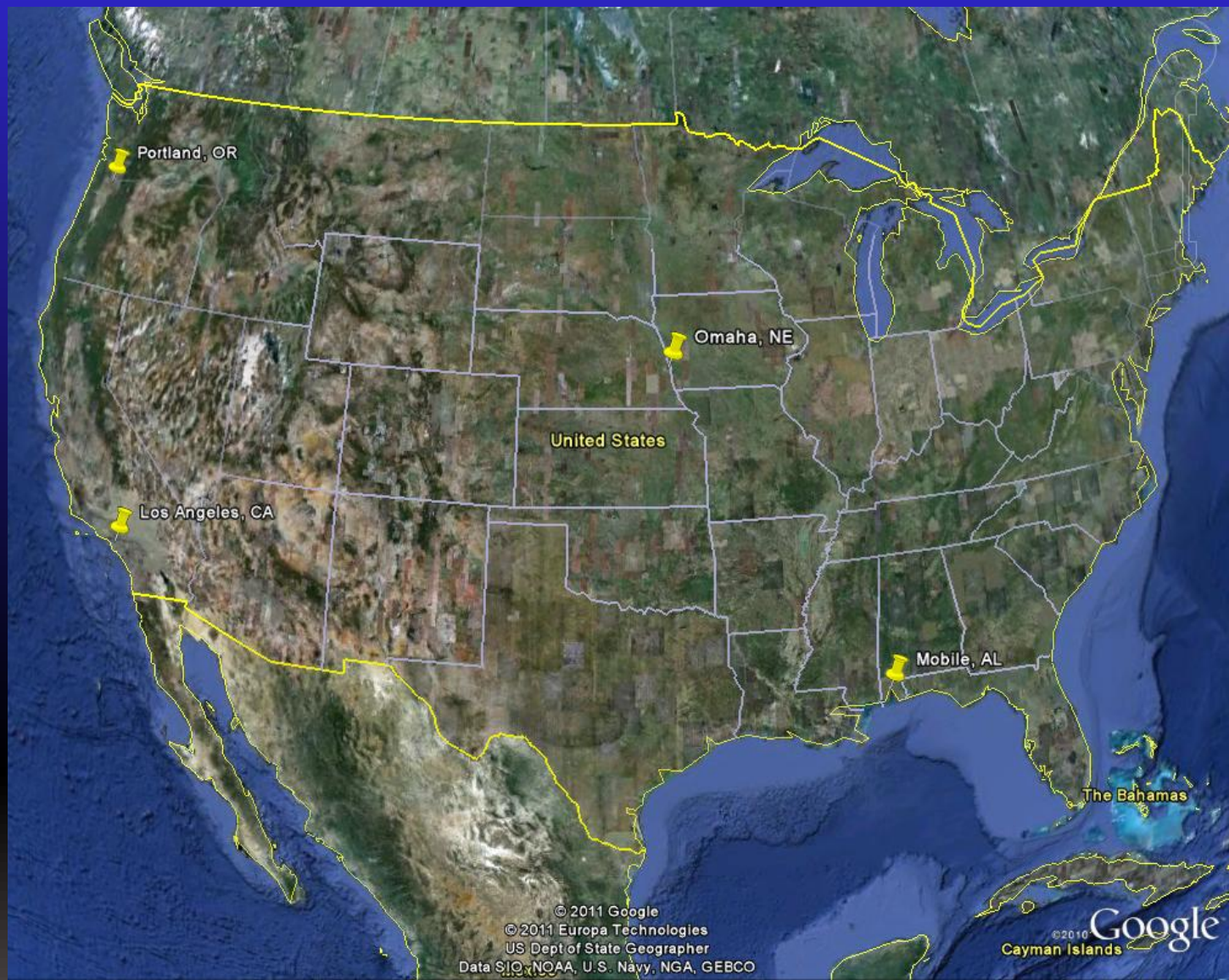


CWMS – Overview

CWMS is an integrated system of hardware, software, and communication resources supporting the U.S. Army Corps of Engineers' real-time water control mission.







CWMS – Overview

Automated data collection via satellites



CWMS suite of hydrologic, operations, and impact analysis models available.

WEST develops and deploys CWMS.

1975

1985

1995

2005

2015

Manual data collection & storage

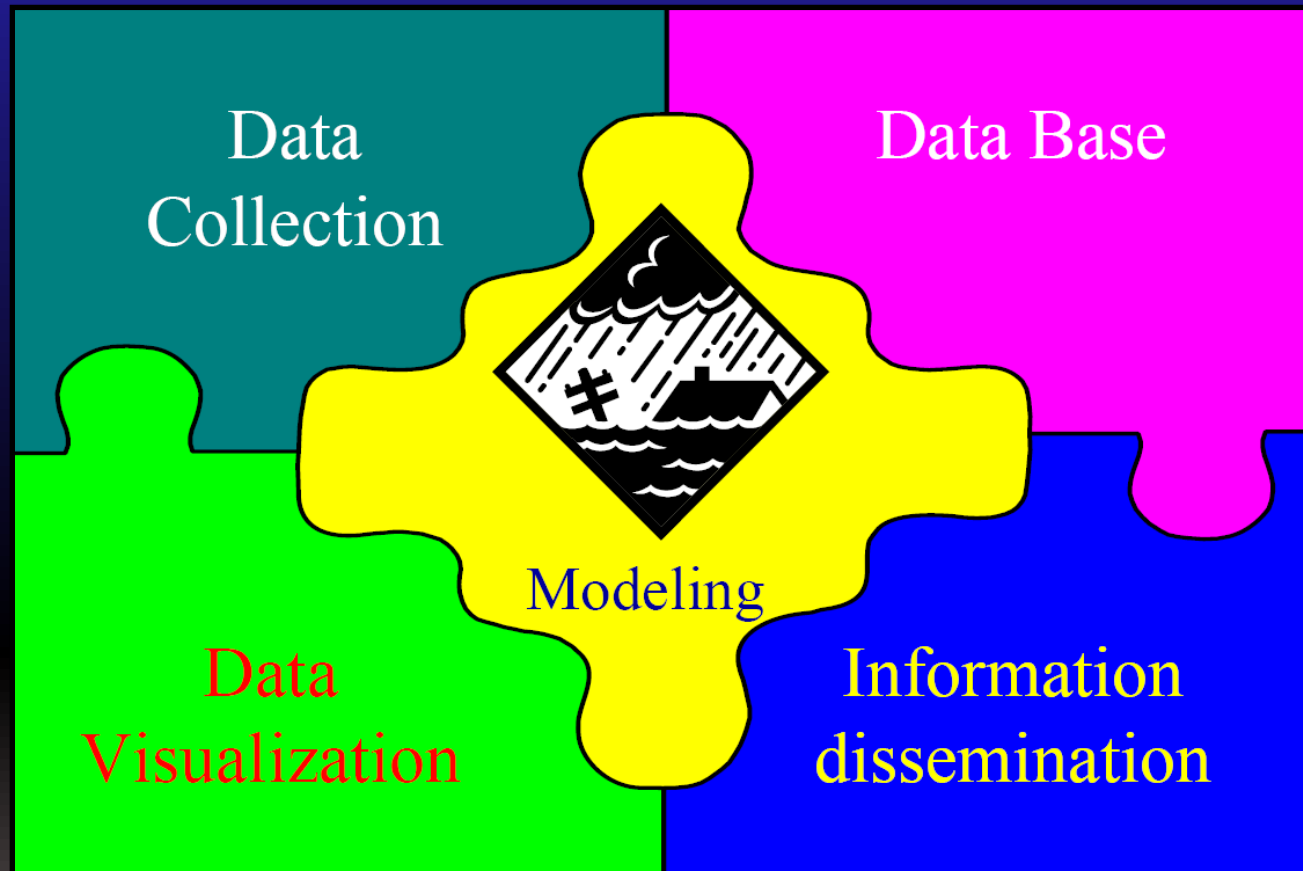
Real-time data handling, WCDS modernization



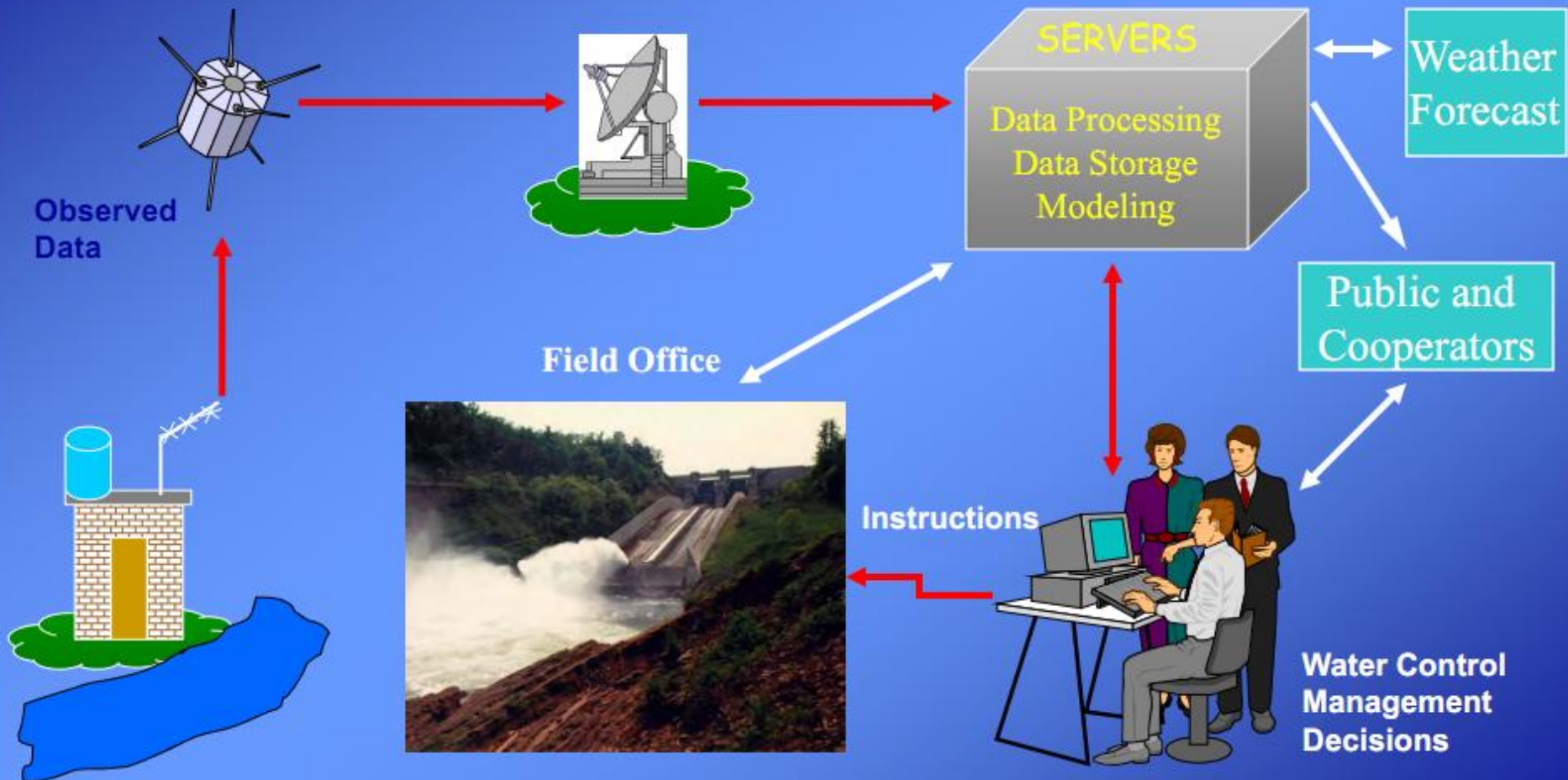
CWMS deployed Corps-wide for all major watersheds.

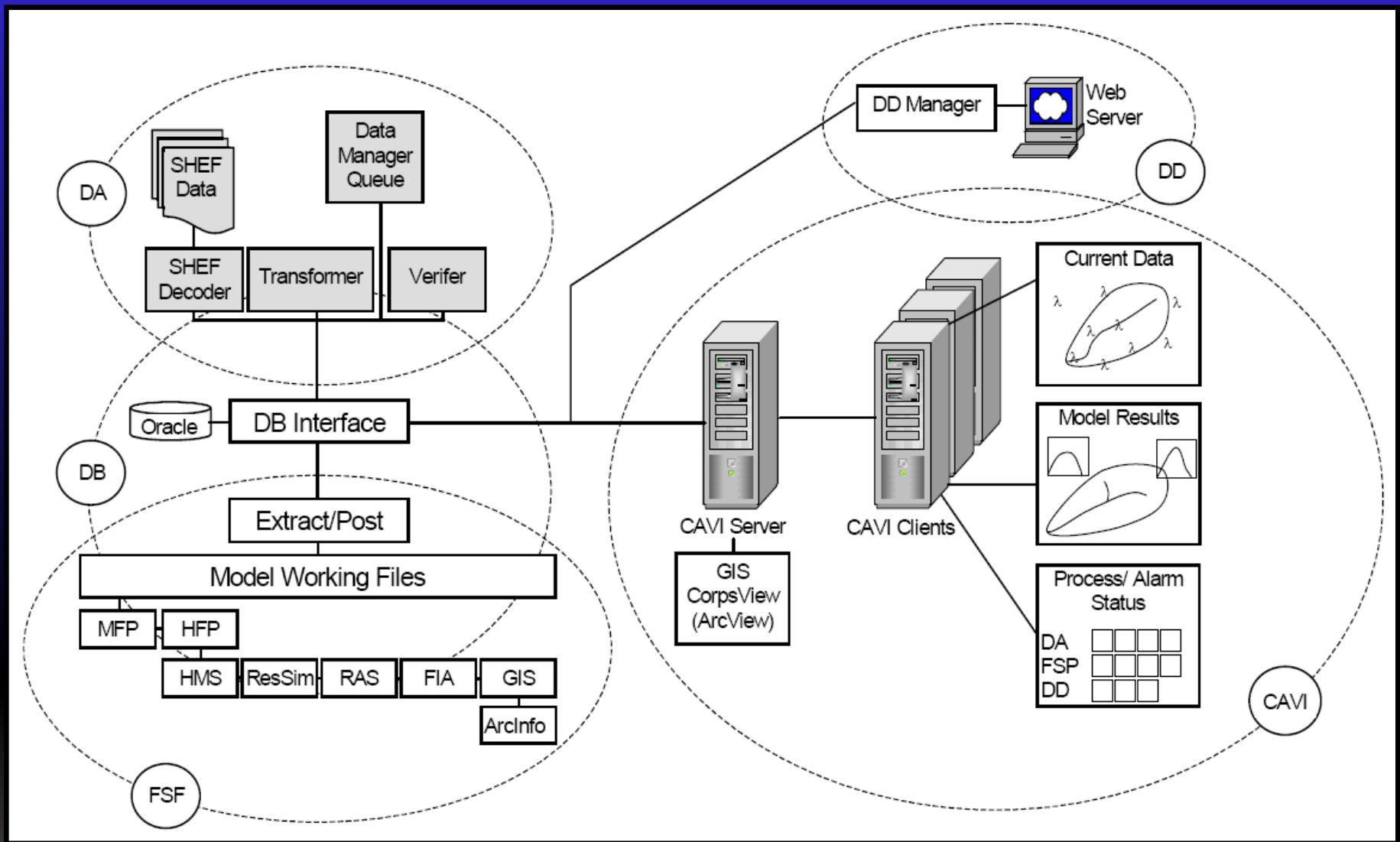


CWMS – Overview



CWMS Software Integrates the Processing from Data to Water Management Decisions





Modeling Components

CWMS provides support for decision making using any combination of the following models:

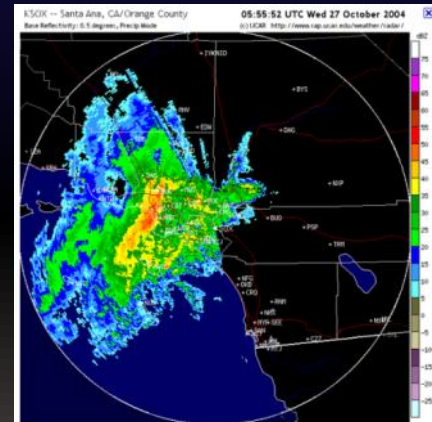
- Meteorology
- Hydrology
- Reservoir operations
- River hydraulics
- Flood impact/economic analysis



Modeling – Meteorology (MFP)

The Meteorological Forecast Processor (MFP) combines observed precipitation with future precipitation scenarios

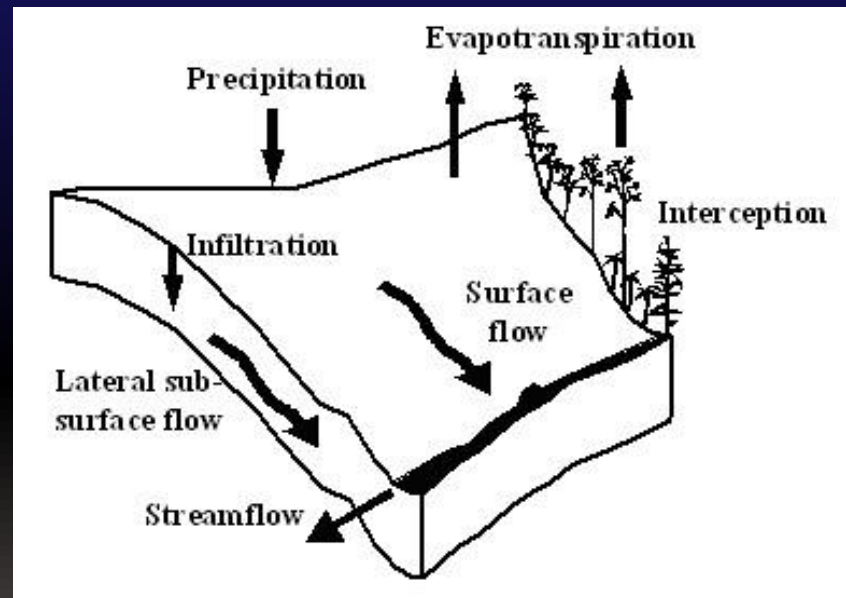
- Observed Precipitation
 - Rain gages (ALERT)
 - Radar based rainfall (NEXRAD)
- Future Precipitation
 - NWS Quantitative Precipitation Forecasts (QPF's)
 - Manual entry



Modeling – HEC-HMS

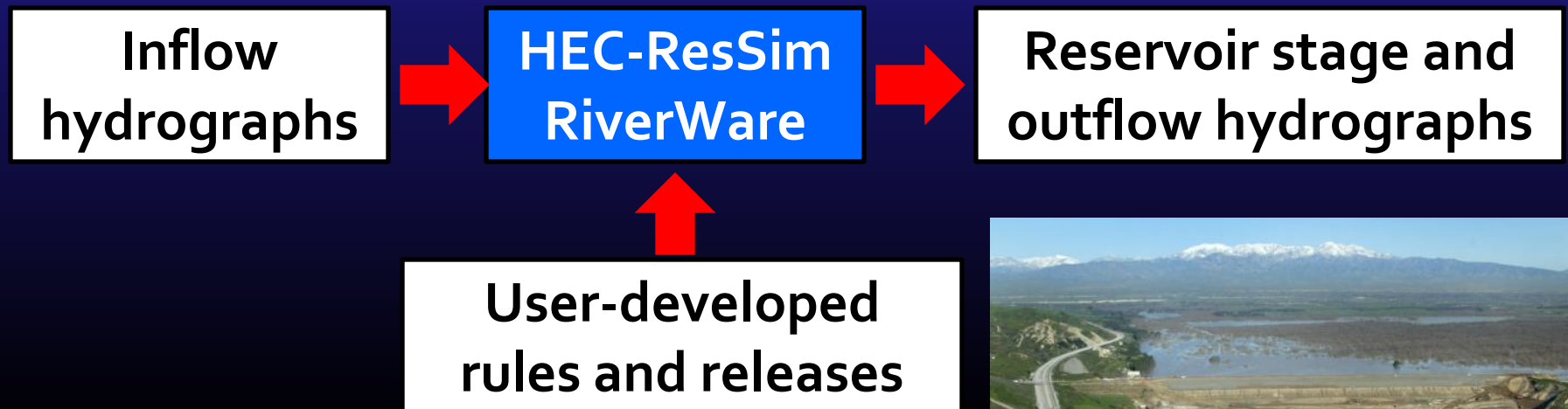
Hydrologic Modeling (HEC-HMS)

- HEC-HMS computes hydrologic forecasts based on precipitation data
- Allows for adjustment of loss and baseflow parameters real-time



Modeling – HEC-ResSim & RiverWare

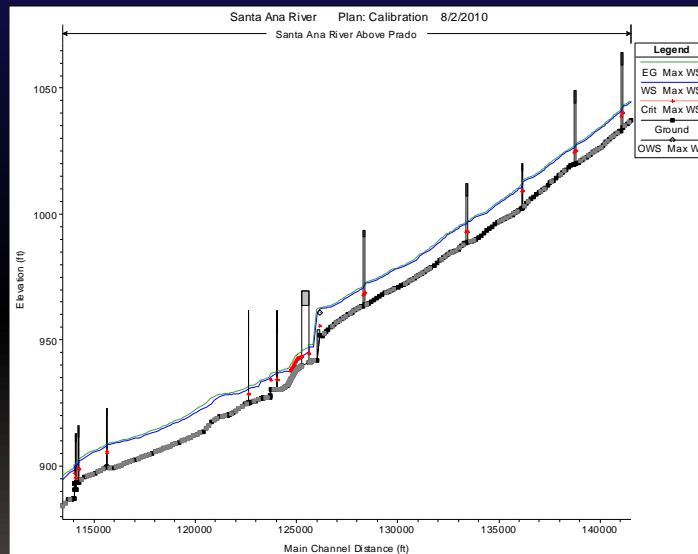
Reservoir Operations modeling using HEC-ResSim or RiverWare



Modeling – HEC-RAS

River Hydraulics – HEC-RAS

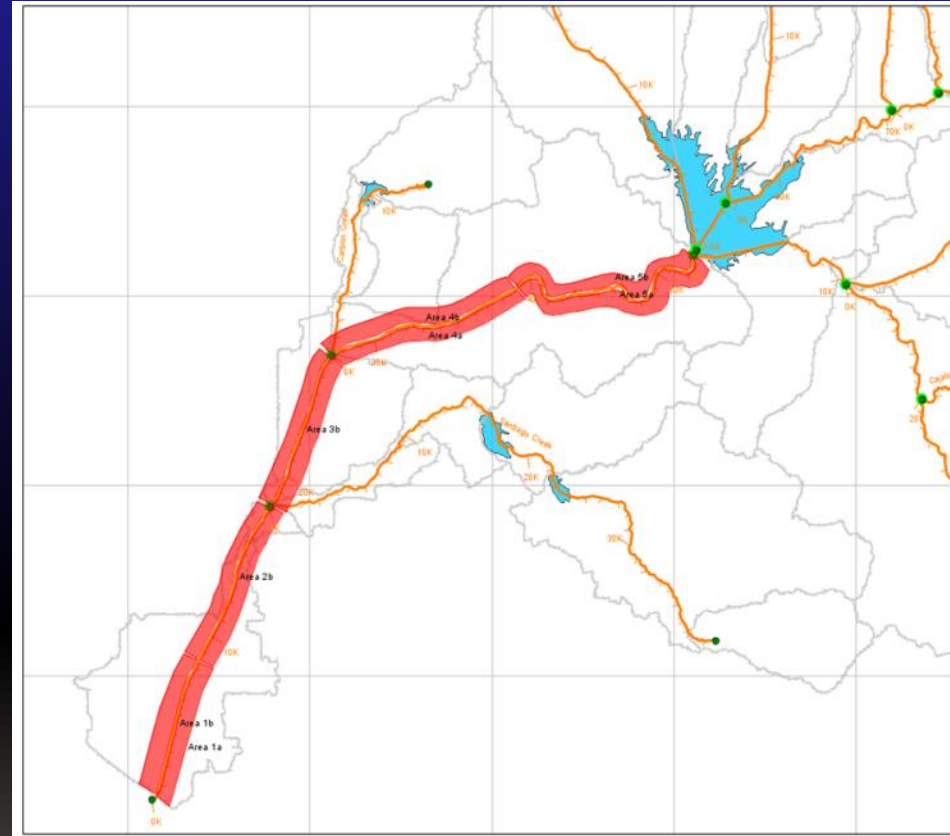
- Computes water depths and velocities
- Steady and unsteady flow analysis available
- Results sent to GIS for inundation boundaries



Modeling – HEC-FIA

Economic /Impact Analysis HEC-FIA

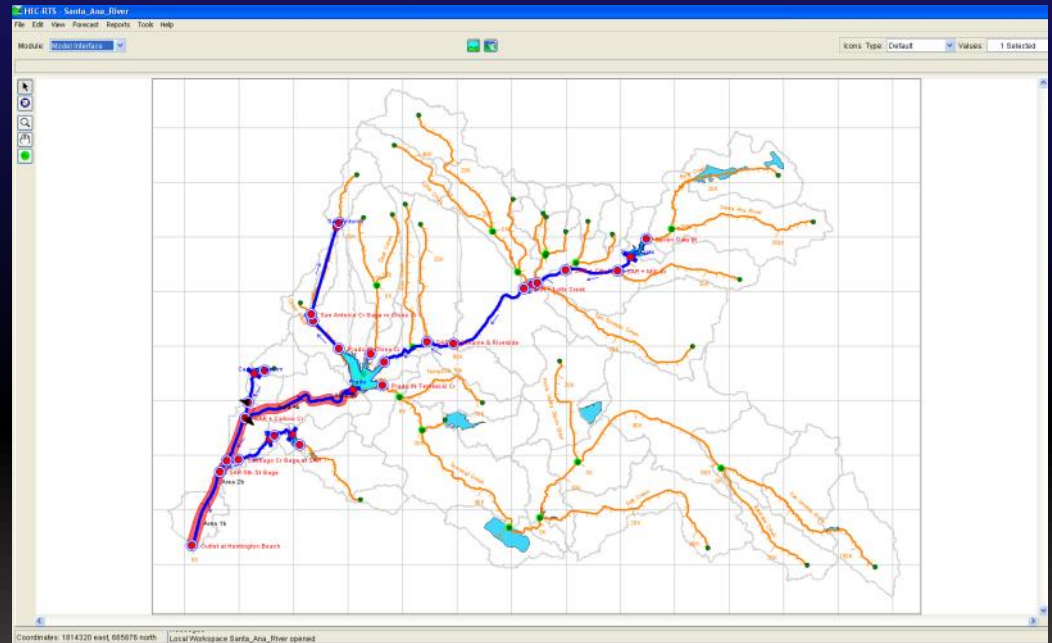
- Impact Areas
- Damages and benefits with and without the project
- Action tables provide instructions for managers during events

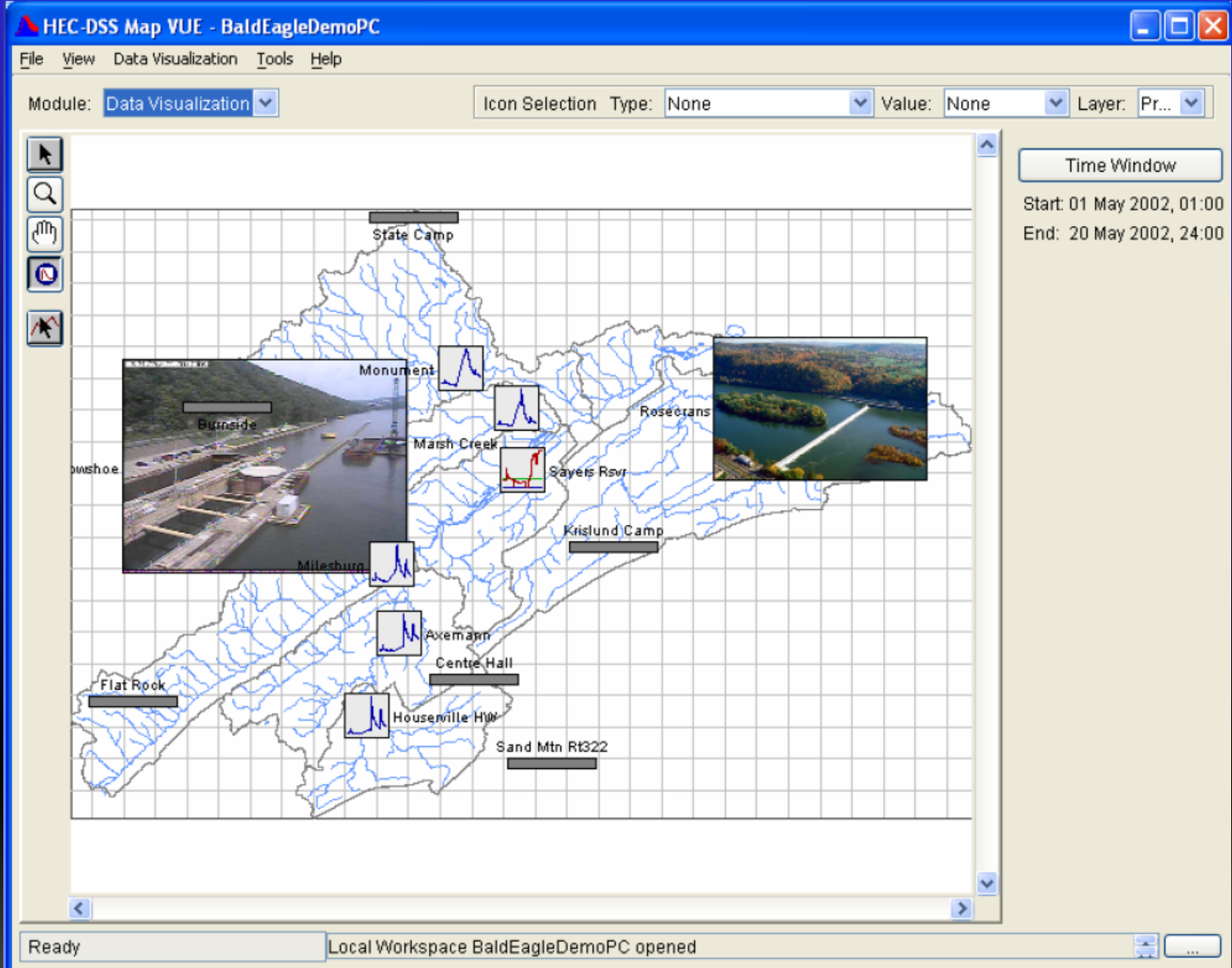


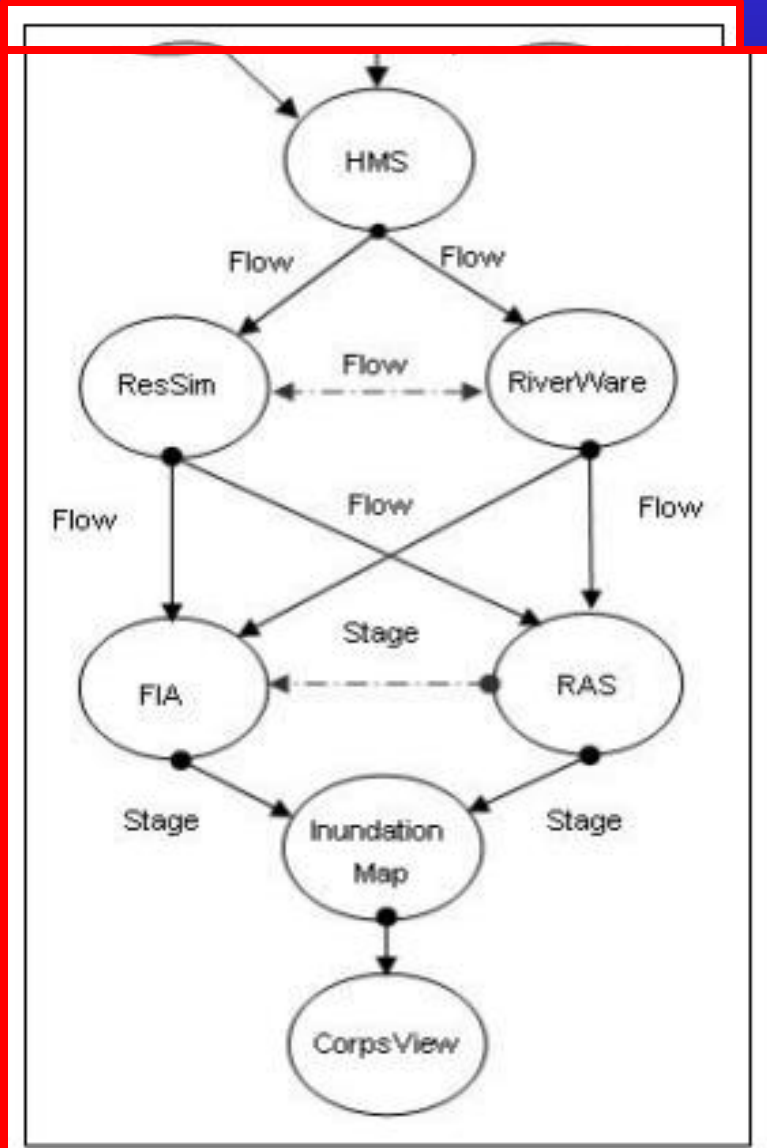
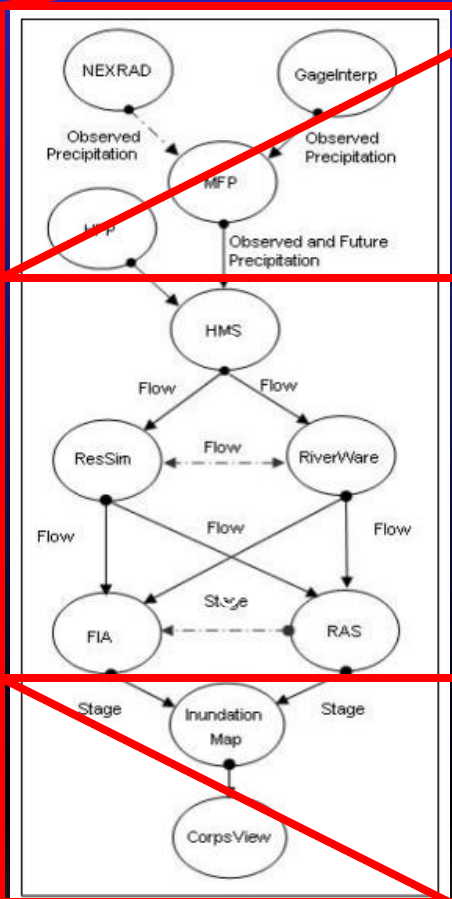
Modules and components

The Control and Visualization Interface (CAVI) is the primary framework of CWMS and controls the other functional modules.

- Data Acquisition Module
- Data Visualization Module
- Model Interface Module
- Watershed Setup Module







Modeling Steps

The modeling process for CWMS is as follows

- Check status and currency of real-time data
- Select a forecast time
- Adjust model parameters to reflect current conditions
- Perform model computations
- View results
- Modify model parameters as necessary
- Re-compute the simulation



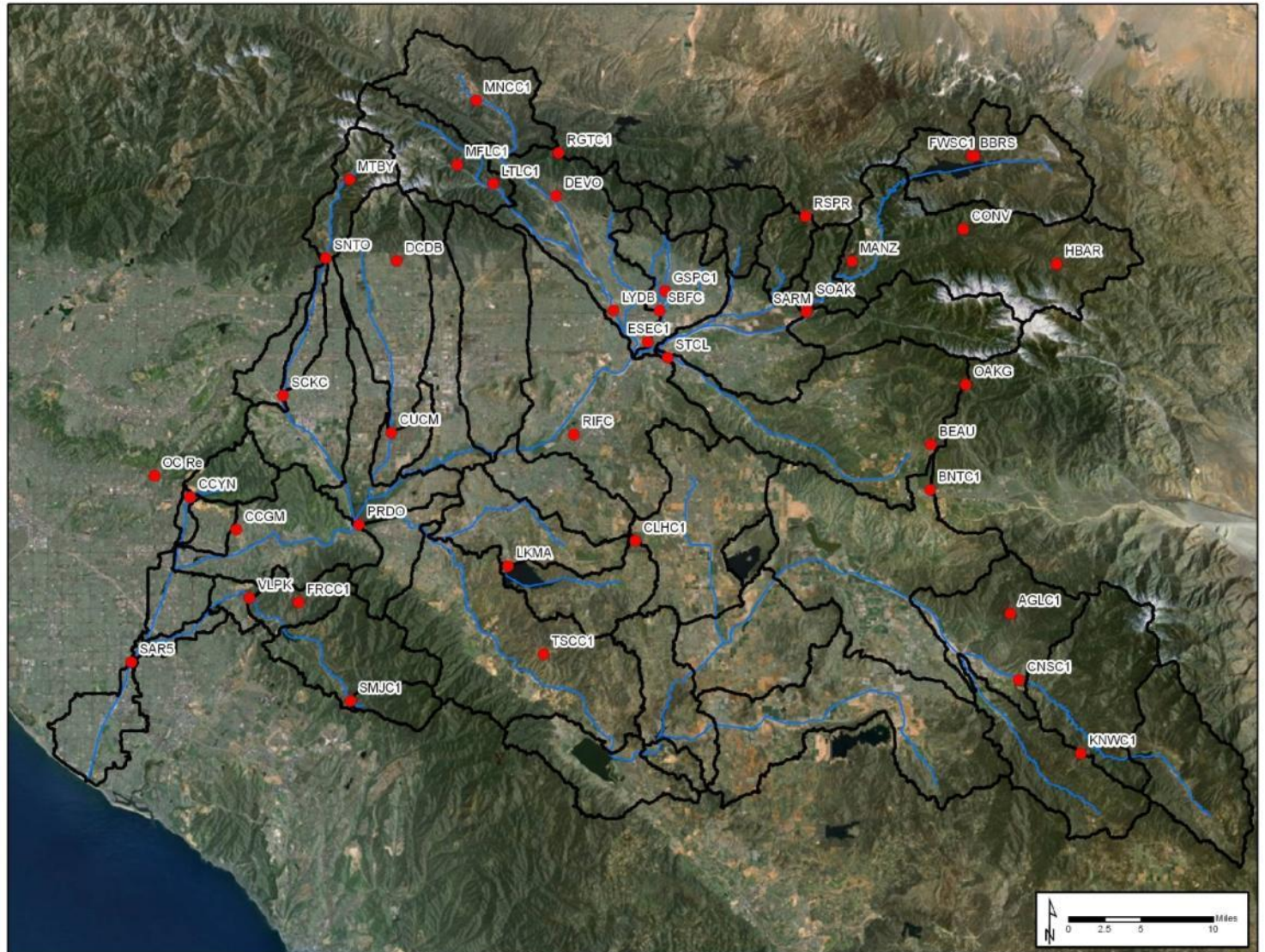
Santa Ana River CWMS

Santa Ana River Watershed

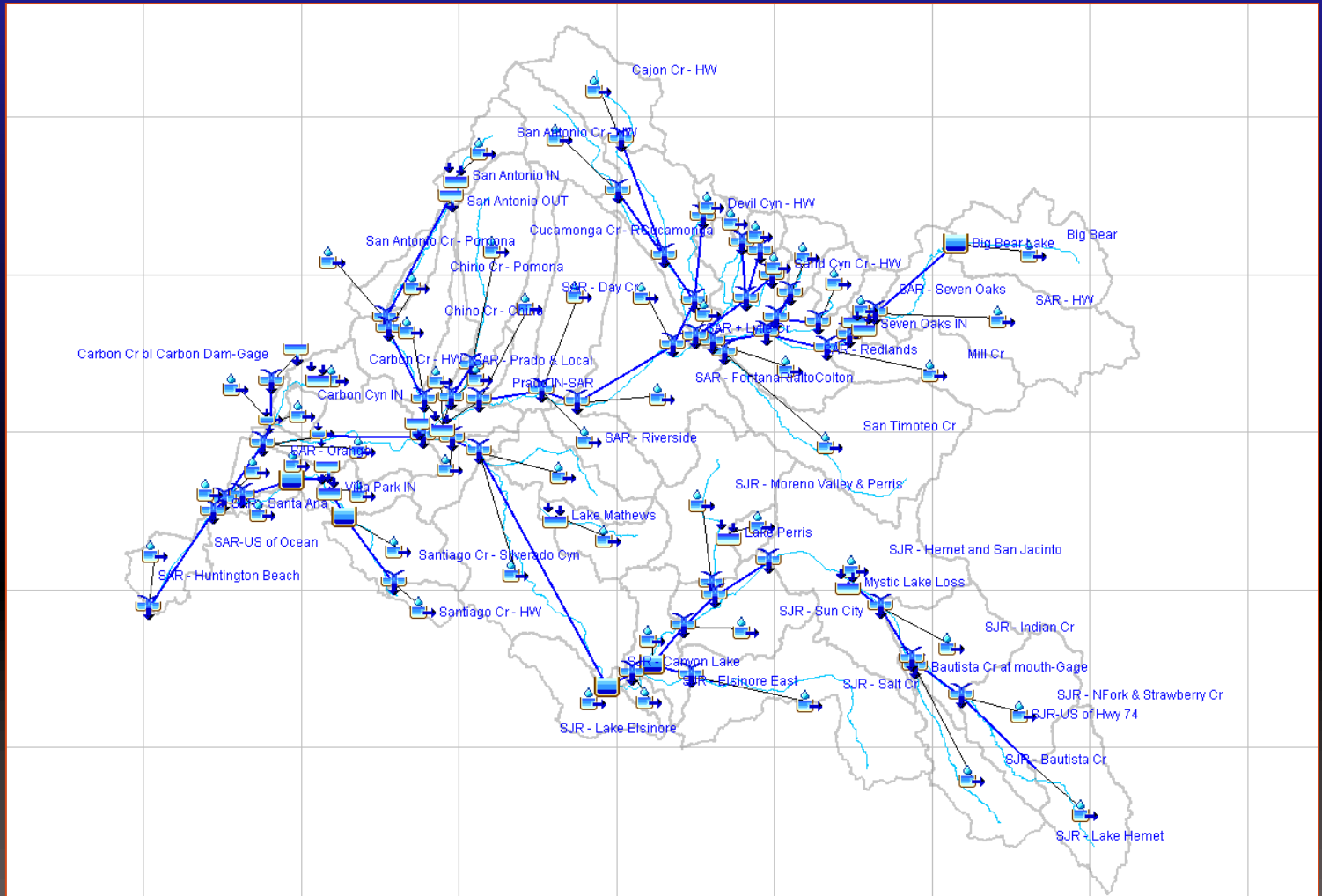
- Drainage Area: 2,500 mi²
- Main Stem: 110 miles long
- Heavily Urban
- Approx. 4.8 million people



Santa Ana River CWMS – MFP



Santa Ana River CWMS – HEC-HMS



[illegible]

Santa Ana River CWMS – HEC-ResSim

Table 1. MINIMUM AND MAXIMUM GATE OPENING REQUIREMENTS		
GATE TYPE	MINIMUM GATE OPENING (FEET)	MAXIMUM GATE OPENING (FEET)
REGULATION OUTLET (R.O.)	.75	6.8
LOW FLOW (L.F.)	.5	2.8

Table 2. RECOMMENDED MAXIMUM RATE OF RELEASE CHANGE		
DISCHARGE	TO INCREASE FLOW	TO DECREASE FLOW
0 - 200	NO RESTRICTION	NO RESTRICTION
UP TO 500	250 CFS/HOUR	250 CFS/HOUR
500 - 4,000	500 CFS/HOUR	500 CFS/HOUR
4,000 - 8,000	1000 CFS/HOUR	1000 CFS/HOUR

MDL - Minimum Discharge Line
 LF - Low Flow Gate
 RO - Regulation Outlet Gates (Main Gates)
 MDLE - Minimum Discharge Line Extension *

* During the dry months, the MDLE will usually be used to bypass the plunge pool. The MDLE is controlled by a 30-inch ball valve. This ball valve cannot be used to regulate flows and must be either in a fully open or fully closed position.

Storage values shown were acquired from year 1999 survey data.

NOTES:

1. **SEDIMENT POOL:**
 - Additional stop logs are installed as necessary prior to each flood season. Sediment pool elevation may vary in any given year.
 - Additional stop logs may be installed during the flood season, if necessary. When necessary, water surface elevation is within this pool, releases are generally made through the MDLE.

2. **DEBRIS POOL:**
 - Prior to rising LF and/or RO gates sluice gate needs to be opened. See Section 7.4b.6 of this document for procedures.

3. **INTERMEDIATE POOL:**
 - Maximum combined capacity of LF and MDL in this elevation range is 500 cfs.

- May delay releases and modify release rates if hydrologic conditions warrant to support mitigation and enhancement plans.

4. **MAIN TRASH RACK POOL:**
 - During Rising Stage: Release 50 cfs through the MDL only.

- During Falling Stage: Release theoretical maximum side rates. The theoretical maximum Q's at different elevation ranges are:

- @2265 ft. NGVD — Q = 500 cfs
- @2299 ft. NGVD — Q = 1,000 cfs
- @2275 ft. NGVD — Q = 1,500 cfs
- @2299 ft. NGVD — Q = 2,000 cfs

- Note that the rates shown can be adjusted depending upon the amount of trash observed, the proximity of the next storm, the time required to clean the trash racks, and operation of the dam.

- May delay releases and modify release rates if hydrologic conditions warrant to support mitigation and enhancement plans.

- See Table 1 for maximum and minimum allowable gate openings.

5. **MAIN POOL:**
 - During Rising Stage: The Q's at different elevation ranges are:

- @2299 ft. NGVD — Q = 2,000 cfs
- @2300 ft. NGVD — Q = 2,000 cfs
- @2400 ft. NGVD — Q = 4,340 cfs
- @2500 ft. NGVD — Q = 6,260 cfs
- @2580 ft. NGVD — Q = 7,000 cfs

- May delay releases and modify release rates if hydrologic conditions warrant to support mitigation and enhancement plans.

- See Table 1 for maximum and minimum allowable gate openings.

6. **SPILLWAY SURCHARGE:**
 - During Rising Stage: Below of 2585 ft. NGVD, maintain a combined release total of 7,000 cfs. Above of 2585 ft. NGVD, all gates shall be closed.

- During Falling Stage: Gates may be adjusted to maintain the resulting maximum spillway flow for quick evacuation of the remaining surcharge pool.

7. **OPERATIONAL CONSIDERATIONS:**
 - Portals release adjustments, see Tables 1 and 2.

- Scheduled releases will be curtailed, if necessary, in order to assure the safe operation of the dam (i.e., avoidance of downstream channel capacity, or any other emergency).

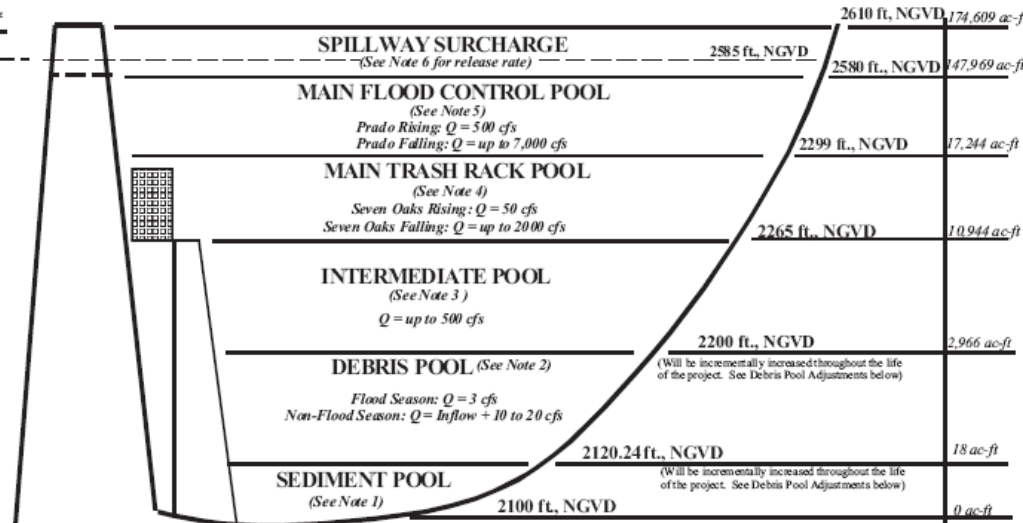
- All release ranges shown can be cut or increased, as necessary, in order to allow safety inspectors for inspection or for maintenance purposes.

- Instrumentation Testing Program: Collection of data to verify the dam's performance may be done if the opportunity exists.

DESIRED GATES TO USE	REQUIRED SLUICE GATE POSITION **
MDL, LF, RO	RIISING: OPEN * FALLING: OPEN *
PRADO RISING: MDL, LF	RIISING: OPEN *
PRADO FALLING: LF, RO	FALLING: OPEN *
SEVEN OAKS RISING: MDL	OPEN
SEVEN OAKS FALLING: MDL, LF, RO	OPEN
MDL & LF	OPEN
MDL & LF	OPEN Once the water level approaches the top of debris pool elevation, sluice gate should be opened, and should remain open throughout the flood season (Refer to Section 7.4b.6 for details).
MDL	CLOSED

* May be closed if necessary. Prior to closure during high flows, however, the LF and RO gates must be temporarily closed to avoid the possibility of damaging the sluice gate.

** Refer to Section 7.4b.6. for procedures in operating the sluice gate.



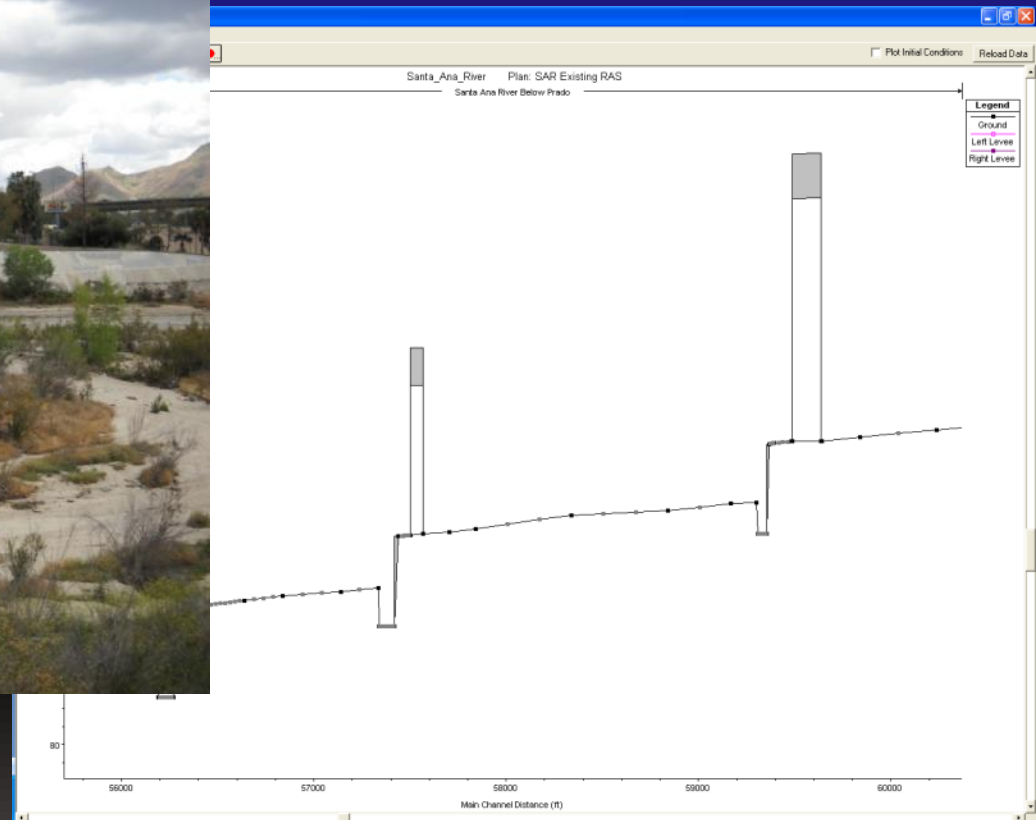
(For detailed drawings of the outlet works features, see Plates 2-06 to 2-24 of this document)

DEBRIS POOL ADJUSTMENTS:

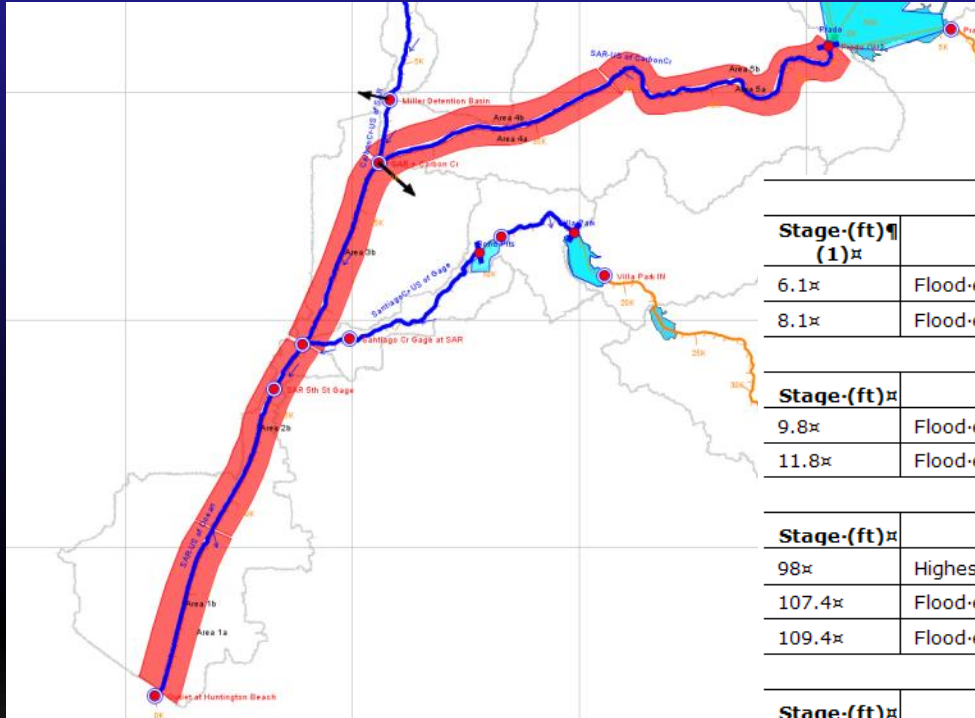
- The maximum allowance for Debris Pool storage is about 3,000 ac-ft. The minimum required Debris Pool storage by the end of project life is about 800 ac-ft.
- As sediments accumulate and additional stop logs are placed within the multislevel withdrawal structure, the top of sediment pool will rise and the debris pool storage will diminish.
- When it is suspected that the debris pool storage is approaching the minimum of 800 ac-ft, the reservoir should be re-surveyed and the top of debris pool elevation raised to re-establish the 3,000 ac-ft of debris pool storage.
- Continue raising the top of debris pool elevation over project life until the top of debris pool reaches the final elevation of 2300 ft. NGVD.

SEVEN OAKS DAM SANTA ANA RIVER BASIN, CALIFORNIA WATER CONTROL MANUAL
WATER CONTROL PLAN
Revised: October 2002
(Note: Revise Plate every time debris pool elevation is increased)
U.S. ARMY CORPS OF ENGINEERS LOS ANGELES DISTRICT

Santa Ana River CWMS – HEC-RAS



Santa Ana River CWMS – HEC-FIA



1a		
Stage-(ft)¶ (1)¶	Flood-Impact¶ (2)¶	Action-Required¶ (3)¶
6.1¶	Flood-elevation within 2-ft-of-top-of-levee¶	Prepare-for-potential levee-overtopping¶
8.1¶	Flood-elevation reaches-top-of-levee¶	Perform-flood-fighting-operations¶
1b		
Stage-(ft)¶	Flood-Impact¶	Action-Required-¶
9.8¶	Flood-elevation within 2-ft-of-top-of-levee¶	Prepare-for-potential levee-overtopping¶
11.8¶	Flood-elevation reaches-top-of-levee¶	Perform-flood-fighting-operations¶
2a		
Stage-(ft)¶	Flood-Impact¶	Action-Required-¶
98¶	Highest stage-on-record¶	None¶
107.4¶	Flood-elevation within 2-ft-of-top-of-levee¶	Prepare-for-potential levee-overtopping¶
109.4¶	Flood-elevation reaches-top-of-levee¶	Perform-flood-fighting-operations¶
2b		
Stage-(ft)¶	Flood-Impact¶	Action-Required-¶
98¶	Highest stage-on-record¶	None¶
107.7¶	Flood-elevation within 2-ft-of-top-of-levee¶	Prepare-for-potential levee-overtopping¶
109.4¶	Flood-elevation reaches-top-of-levee¶	Perform-flood-fighting-operations¶

Questions?

